

November / December 2021

a)

$$m\ddot{z} = f_{\text{net}} - mg$$

b)

$$\text{Let } f = f_{\text{net}} - mg$$

$$m\ddot{z} = (mg + f) - mg$$

$$m\ddot{z} = f$$

Laplace transform

$$ms^2 Z - ms z(0) - m s z'(0) = F$$

Assume $z(0)$ and $z'(0) = 0$

$$ms^2 Z = F$$

$$\frac{Z}{F} = \frac{1}{ms^2}$$

c)

$$\text{CLTF: } \frac{\frac{k}{ms^2}}{\frac{k}{ms^2} + 1} = \frac{k}{k + ms^2}$$

d)

$$\text{Let } m=1, k=9$$

$$\frac{Z}{R} = \frac{9}{9+s^2} = \frac{3}{s^2+3^2}$$

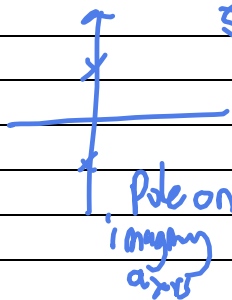
Stability check \rightarrow $CLT: s^2 + 9 = 0$

1) Routh Hurwitz

s^2	1	3
s	0	0
k		

\leftarrow marginally stable

2) Plot roots



Therefore the system is marginally stable.

Since it is marginally stable with no steady state output therefore there is no steady state error.



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d) $\frac{Z}{R} = \frac{9}{s^2+9}$ Apply unit ramp $Z = \frac{9}{s^2+9} \left(\frac{1}{s^2} \right)$

Apply partial fraction

$$Z = \frac{1}{s^2} - \frac{1}{s^2+9}$$

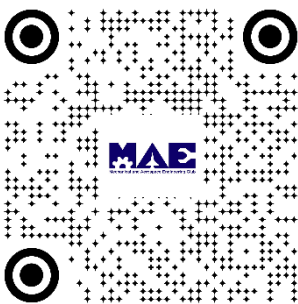
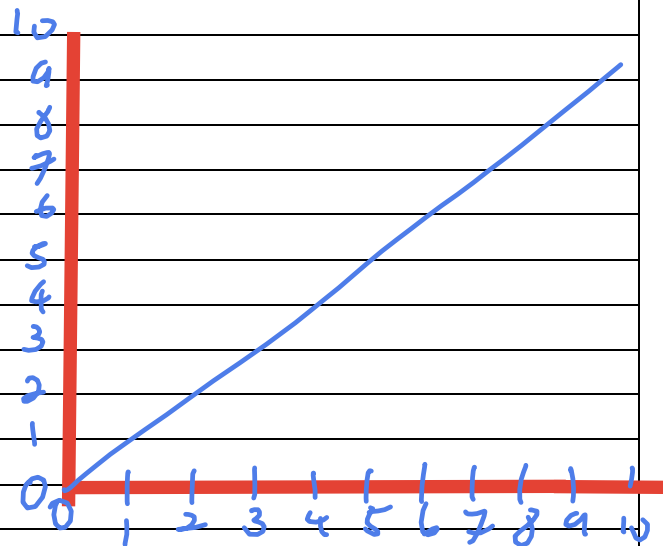
$$Z = \frac{1}{s^2} - \frac{1}{3} \left(\frac{3}{s^2+3^2} \right)$$

Apply Inverse Laplace

$$z(t) = t - \frac{1}{3} \sin 3t$$

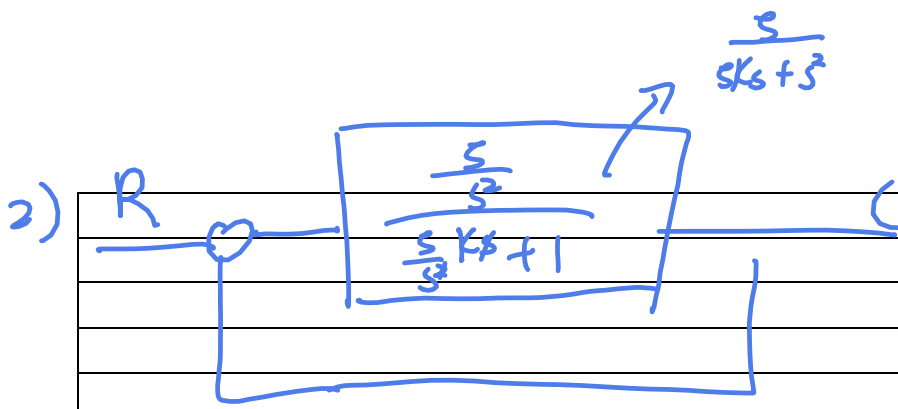
e) $t \quad z(t) = t - \frac{1}{3} \sin 3t$

0	0
1	0.95
2	2.09
3	2.86
4	4.17
5	4.78
6	6.25
7	6.72
8	8.3
9	8.68
10	10.324



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$$\text{OLTF: } \frac{C}{R} = \frac{\frac{s}{s^2} \cdot \frac{s}{s^2 + 1}}{\frac{s}{s^2 + 1} + 1} = \frac{s}{s^2 + sK + 1}$$

b) CE: $s^2 + sK + 1$

Routh Hurwitz

s^2	1	1	$sK > 0$
s	sK	0	$K > 0$
k	1		

c) OLTF: $\frac{s}{s^2 + 15s} = \frac{s}{s(s + 15)} = \frac{1}{s + 15}$

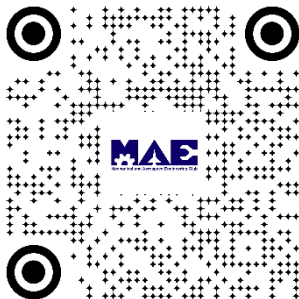
Type 1, unit step input

$$e_{ss} = 0$$

d) Type 1, unit ramp input, $\rightarrow e_{ss} = \frac{1}{K_v}$

$$K_v = \lim_{s \rightarrow 0} s G(s) = \lim_{s \rightarrow 0} \frac{s}{s(sK + s)} = \lim_{s \rightarrow 0} \frac{s}{sK + s} = \frac{1}{K}$$

$$e_{ss} = 0.2 = \frac{1}{K}, \quad K = 0.2 \#$$



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e) $M_p = 2\%$ overshoot

$$\xi = \frac{-\ln(M_p)}{\sqrt{\pi^2 + \ln^2(M_p)}} \xrightarrow{0.02}$$

$$\xi = 0.7797 \xrightarrow{0.02}$$

$$\frac{C}{R} = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$\frac{C}{R} = \frac{5}{s^2 + 5Ks + 5}$$

$$\omega_n^2 = 5$$

$$\omega_n = \sqrt{5}$$

$$5K = 2\xi\omega_n$$

$$K = \frac{2(0.7797)(\sqrt{5})}{5}$$

$$= 0.6973\#$$

3) When $G_c(s) = K$

$$OLTF = \frac{Ks}{(s^2 + 4s + 8)(s + 2)}$$

Zero: $s = 0$

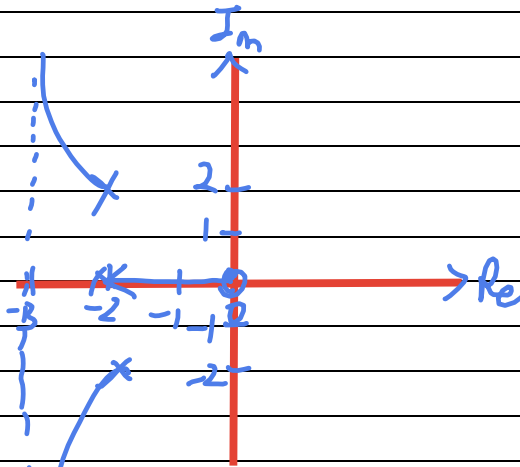
Poles: $s^2 + 4s + 8 = 0$

Pole 1: $s = -2 + 2j$

Pole 2: $s = -2 - 2j$

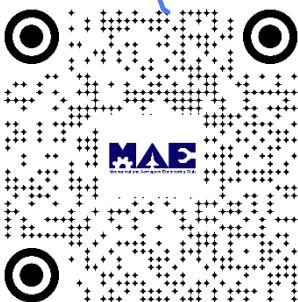
Pole 3: $s = -2$

pole zero asymptote
 $\frac{3}{-1} = 2$



$$\sigma = \frac{-2 - 2 - 2}{3}$$

$$= -3$$



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coefficient determine location of the desired pole

$$b) A e^{-\zeta \omega_n t} \cos(\omega_n t + \phi)$$

↳ equals to $s = -\zeta + j$

PID controller

$$G_{cc} = K_D (s + z_1) \frac{(s + z_2)}{s}$$

$$OLTF = \frac{K_D (s + z_1) (s + z_2)}{s (s^2 + 4s + 8) (s + 2)}$$

Let $z_1 = 2$ (so that you can cross out the other pole)

$$OLTF = \frac{K_D (s + z_2)}{(s^2 + 4s + 8) (s + 2)}$$

$$CLTF = \frac{K_D (s + z_2)}{s^2 + 4s + 8 + K_D (s + z_2)}$$

$$CE = (s^2 + 4s + 8) + K_D (s + z_2) = 0$$

Subs desired pole $s = -5 + j$

$$(12 - 6j) + K_D (-5 + j + z_2) = 0$$

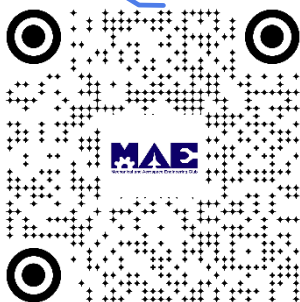
$$12 - 6j - 5K_D + K_D j + K_D z_2 = 0$$

$$(12 - 5K_D + K_D z_2) + (-6 + K_D)j = 0$$

$$12 - 5(6) + (6)z_2 = 0 \quad K_D = 6$$

$$z_2 = 3$$

$$OLTF = \frac{6 (s + 3)}{s^2 + 4s + 8}$$



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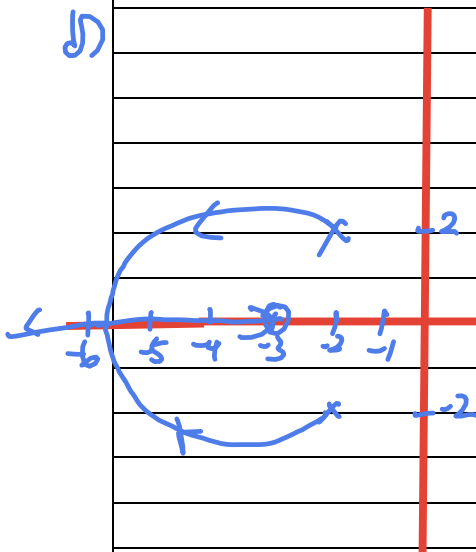
c) No, both conditions cannot be fully satisfied
 Based on the O.T.F of the PID controller, it is
 a type 0 system, $e_{ss} = \frac{1}{1+K_p} = \frac{1}{1+0.25} = 0.8$

$$K_p = \lim_{s \rightarrow 0} \frac{6(s+3)}{(s^2+4s+8)}$$

$$= \frac{6(3)}{8} = 0.25$$

You can have the desired transient response but not the steady state response.

d)

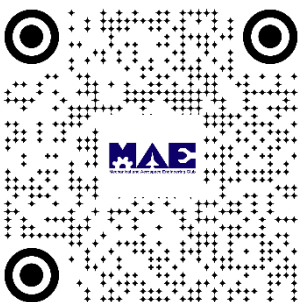


Zero: $s = -3$
 Pole: $P_1: s = -2 + 2j$
 $P_2: s = -2 - 2j$

Asymptote
 $\sigma = \frac{(-2-2) - (-3)}{2} = -7$

Break in part
 $(s^2+4s+8) + K(s+3) = 0$
 $K = -\frac{(s+3)}{(s^2+4s+8)}$

$\frac{dK}{ds} = 0$
 $0 = (2s+4)(s+3) - (1)(s^2+4s+8)$
 $0 = 2s^2 + 6s + 12 - (s^2 + 4s + 8)$
 $0 = s^2 + 2s + 4$
 $s = -5.236, s = -0.764$
 (negative)



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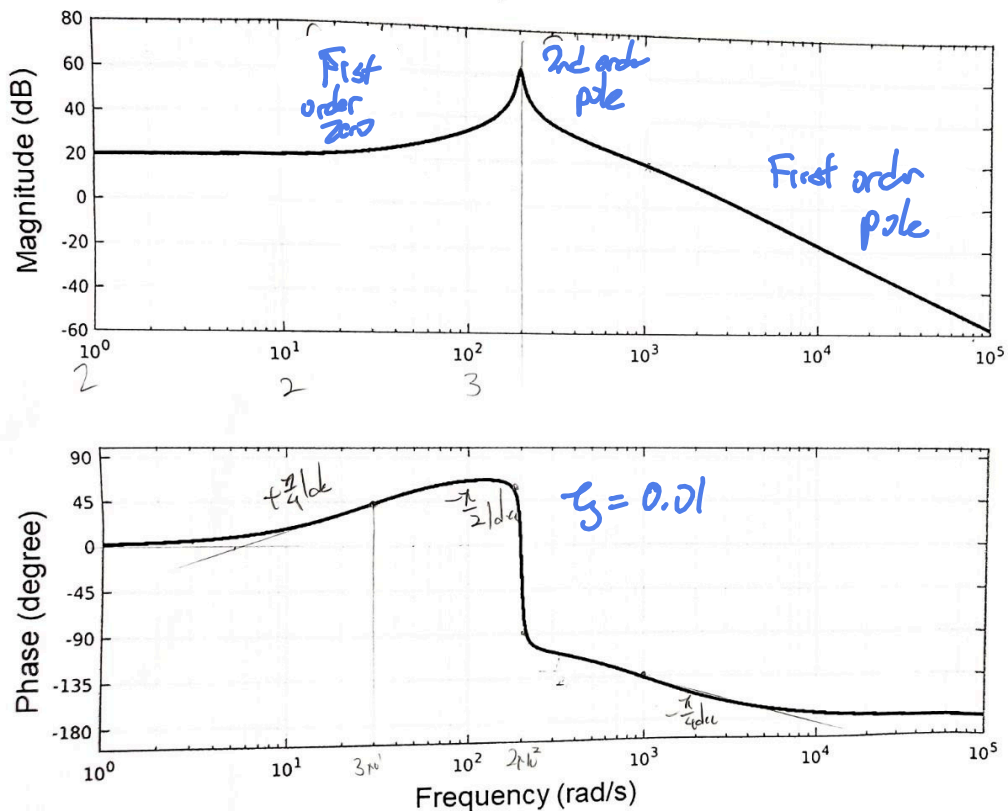
e) i) As k increases, the ζ damped ratio increases, the system stop oscillating, the overshoot of the system decreases.

ii) All roots in LHP, Hence stable

iii) Large k , Larger K_p , smaller e_{ss} , e_{ss} tends to 0

iv) As k increases, the ζ damped ratio increases, system becomes overdamped, Hence 2nd settling time increases

4)



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a) Check intercept

$$20 \lim_{s \rightarrow 0} G(s) = 20 \quad \lim_{s \rightarrow 0} G(s) = 10'$$

$$K = 10$$

No slope

First order zero at $\omega = 30$

Second order pole at $\omega = 2 \times 10^3 = 2000$

First order pole at $\omega = 1 \times 10^3 = 1000$

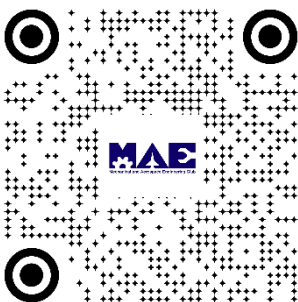
$$G(s) = 10 \left(\frac{s+30}{30} \right) \left(\frac{200^2}{s^2 + (9.01)(200)s + 200^2} \right) \left(\frac{1000}{s+1000} \right)$$
$$= \frac{13333.33 (s+30)}{(s^2 + 2s + 200^2)(s+1000)}$$

b) i) System is stable because all poles in RHP
 $s^2 + 2s + 200^2$, $s = -1 \pm j199.9975$ (Pole 1, pole 2)
 $s + 1000$, $s = -1000$ (Pole 3)

ii) System type 0, $e_{ss} = \frac{1}{1+K_p}$

$$\lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{13333.33 (s+30)}{(s^2 + 2s + 200^2)(s+1000)} = 9.9999$$

iii) System type 0, not ramp, $e_{ss} = \infty$



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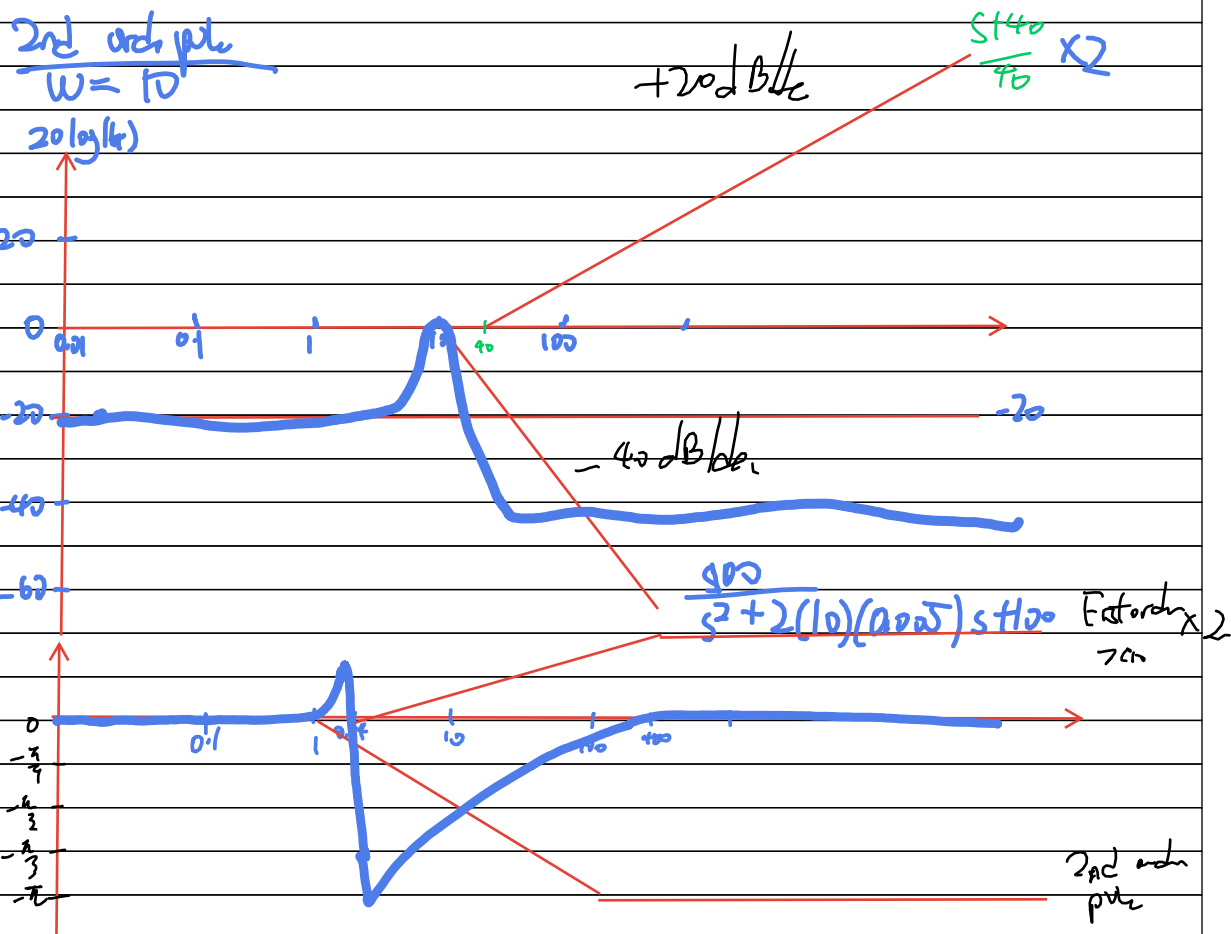
$$G_2(s) = \frac{(s+40)^2}{160(s^2+2(10)(0.005)s+10^2)} = \frac{(s+40)(s+40)}{160(s^2+2(10)(0.005)s+10^2)}$$

$$= \frac{(40^2)}{(160)(10^2)} \left(\frac{s+40}{40}\right) \left(\frac{s+40}{40}\right) \frac{10^2}{(s^2+2(10)(0.005)s+10^2)}$$

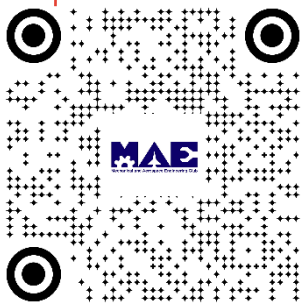
$$\approx 0.1 \left(\frac{s+40}{40}\right) \left(\frac{s+40}{40}\right) \frac{100}{s^2+2(10)(0.005)s+10^2}$$

Intercept:
 $20 \log |0.1| = -20$

First order zero
 $\frac{s+40}{40}, \omega = 40$



All the best PSZ :)



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